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Mechanical Design of MI8 Collimators

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Abstract

A collimation system for the Booster to Main Injector transfer line (MI8 line) has been designed and installed at MI-836 and MI-838. This system will remove particles in the beam halo from 8 GeV Booster beam before it arrives at the Main Injector. A pair of 5 ton collimators, with horizontal and vertical motion, is installed between the gradient magnets in half-cell 836 and an identical system is placed one cell away (about 90° in phase advance) at 838. A description of the mechanical structure of the collimator, including the support and motion control is provided. The vacuum, loss monitor (LM), beam position monitor (BPM), and thermocouple monitoring systems are briefly described.

Introduction

In expectation of increased beam intensity requirements associated with operation of the NuMI beamline, Residual radiation around the Main Injector tunnel was examined prior to the 2004 Fermilab facility shutdown¹. A small but significant contributor to the residual radiation was losses of beam due to tails of the Booster beam which were not accelerated but were scraped around the Main Injector at locations which had only very little less aperture than other similar lattice locations. By providing a more defined beam from the Booster, we will reduce the losses from these tails which will reduce substantially the number of hot locations in the MI Ring. Collimation in the MI8 Line can provide this improved beam to the Main Injector². Tails from the Booster Beam may contribute residual radiation at other, as yet unidentified Main Injector locations. In addition to more general sources of beam tails, measurements of the beam motion induced by changes in the beam trajectory through the Booster Extraction Septum (MP02) suggest that non-uniformity of the fields in this bending magnet (including quadrupole and skew sextupole terms) may be sufficient to create halo from some of the extracted Booster beam³. The design concept for this collimator system is based on the Booster Beam Collimation system⁴. The difference between circulating and single pass beam collimation requires additional collimators. For symmetric collimation, it will be useful and perhaps sufficient to remove only a small fraction of the beam. Beam motion will cause asymmetric scraping of a more intense part of the beam nearer the core. An autotune scheme will be used to minimize the motion. Since four collimators are required, a compact design using 5 tons per collimator was selected despite its lower capacity for shielding beam loss in order to reduce the demands on the motion system. A marble shield surrounds the steel collimator. It is much less susceptible to activation and provides shielding for the MeV gamma rays emitted by activated iron, resulting in a much lower exposure from residual radiation for personnel working in the tunnel. With this design choice, the radiation induced in the tunnel walls and surrounding materials limits the operational loss capability due to radiation which can be extracted into the surface waters. Loss limitations from other criteria are less restrictive.

MI8 Collimator Layout

The MI8 Collimators will intercept the beam in stainless steel vacuum boxes (part of the MI8 vacuum system) surrounded by massive steel absorbers with an external marble shield. As in the Booster collimation system, the motion system will be external to the entire collimator system. A pair of these remotely positioned collimators will be placed in a 5.2 m (200") open space in an MI8 half-cell in which the focusing is provided by gradient magnets. One collimator will provide scraping on one horizontal and one vertical edge (bottom and outside, for example) while the next will scrape the other sides (e.g. top and inside). They will be followed by a fixed collimation mask which will protect the downstream magnet. In order to

scrape large emittance particles which happen to be at small displacement but large angle at the 836 location (initial collimator), a second collimator-mask set will be placed two half cells downstream at 838 (about 90 degrees phase advance). The four collimators are of the same design and each can be used to provide scraping on one side or any corner.

The following table is extracted from the new lattice description of the MI8 Line.

	I	Ī	
Туре	Device	Distance from MI101	Distance from MP02
		meters	meters
Bend	MP02	-754.366	0
Bend	PGD_836A	-257.768	496.598
Trim	HT836	-253.574	500.792
SWIC	MW836	-253.069	501.297
BPM	HP836	-252.599	501.767
Bend	PGD_836B	-252.282	502.084
BPM	VP836	-247.824	506.542
Marker	COL836A	-247.367	506.999
Marker	COL836B	-246.681	507.685
BPM	HP837	-245.665	508.701
Bend	PGD_837A	-243.126	511.24
Trim	VT837	-238.932	515.434
BPM	VP837	-237.589	516.777
Bend	PGD_837B	-237.271	517.095
Bend	PGD_838A	-228.115	526.251
Trim	HT838	-223.921	530.445
BPM	HP838	-222.578	531.788
Bend	PGD_838B	-222.261	532.105
BPM	VP838	-217.803	536.563
Marker	COL838A	-217.346	537.02
Marker	COL838B	-216.66	537.706
BPM	HP839	-215.644	538.722
Bend	PGD_839A	-213.105	541.261
Marker	MQ101U	0	754.366

Collimator Design, Input to Mechanical Design

Preliminary calculations examined the radiation implications of a 12 ton collimator, finding that a more compact design was suitable. After an intermediate design round, the following concept was provided as input to the mechanical design. The collimators as built replace some marble with iron needed for support.

Conceptual design of the MI-8 Collimator is based on the Booster Collimator design. A 2"x2" aperture is surrounded by a 0.75" stainless steel primary absorber (3.5"x3.5" outside by 47.5" long). The bulk of the collimator consists of 35" long iron absorber which is 26" wide by 20" high. This is surrounded by 4 layers of marble which is 3 cm thick (4.72 inches). It was planned to use 1.25" marble which would have provided 5" thickness and 45" length. The marble is held in place by a frame of 1.5" aluminum channels.

		1 (Ollimai Col	iiiiatoi Compoi	icits			
Material	Horizontal	Vertical	Horizontal	Vertical	Length	Weight	
	Edge	Edge	Thickness	Thickness		Lbs	
Vacuum	1"	1"			47.5"	0	
Stainless Steel	1.75"	1.75"	0.75"	0.75"	47.5"	125	
Steel	13"	10"	11.25"	8.25"	35"	5750	
Marble (side)	17.72"	14.72"	4.72"	4.72"	35"	2002	
Marble (2 ends)	18"	15"	16.25"	16.26"	4.72"	2802	

Nominal Collimator Components

The final design included: Support plate 36"x40"x1.75" - weight 700 Lbs

Base plate 38"x 45"x 1.5" – weight 600 Lbs.

Weight to lift: \sim 9300 Lbs. Total weight: \sim 10000 Lbs.

Collimator Design, Overview

Four lifting jacks mounted on the base plate (item 1) provide vertical motion. Travel nuts for these jacks are bolted to the support plate (item 2). THK linear bearing systems mounted onto a support plate permit horizontal movement. The motor, gear box, and 2 ton Uni-Lift Jacks supply the horizontal motion of +/- 1.00" for the vacuum liner (item 3) surrounded with steel absorber (item 4) and marble (item 5). The vertical movement of the collimator from the center of the beam line is +/- 1.00" also. A short bellows (items 6) is joined to the beam pipe (upstream and downstream) and a long bellows (item 7) is installed between two collimators to make a collimation system pair (See Fig.2). Note that no additions to the MI8 vacuum pumping or monitoring were required.

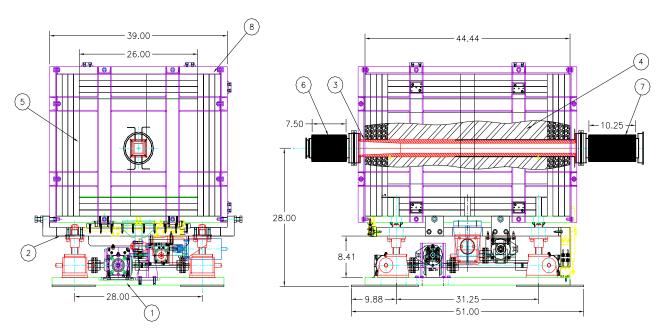


Fig.1. Collimator Assembly.

1- Base Plate Assembly; 2 - Support Plate Assembly; 3 - Vacuum Liner Weldment;

- 4 Steel Shielding Block Assembly; 5 Marble plates; 6 7.5" Bellows Weldment;
- 7 10.25" Bellows Weldment; 8 Aluminum Frame.

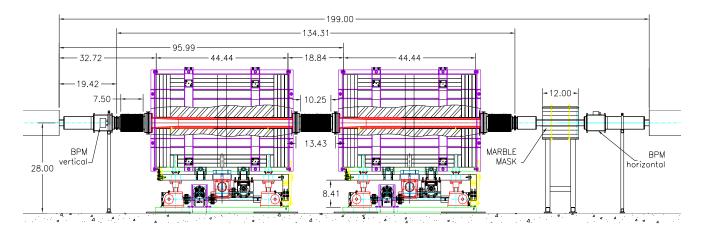


Fig.2 Collimation system layout in 8 Gev line tunnel at MI836 and MI838.

The marble mask surrounds the Recycler-style elliptical beam pipe in the down stream end of the collimation system. Two BPMs are welded into beam line, vertical upstream and horizontal downstream (See Fig.2). Two of the standard gas-filled loss monitors will be employed with each collimator but their placement will be established operationally. The channels I:LM8C1 and I:LM8C2 are assigned to the monitors at 836 while I:LM8C3 and I:LM8C4 are for the 838 monitors.

On a console parameter page, these loss monitor devices appear as follows:

I:LM8C1	LOSSMON @ 836 COLL SYS1
I:LM8C2	LOSSMON @ 836 COLL SYS2
I:LM8C3	$LOSSMON @ 838 \ COLL \ SYS1$
I:LM8C4	LOSSMON @ 838 COLL SYS2

Vacuum Liner

The Vacuum liner is welded from two tapered 304 stainless steel blocks (item 2), circular upstream (item 4) and down stream (item 3) end plates and standard 6" BOOSTER QD Flanges (item 1). The steel blocks create a device with a 2" square vacuum aperture and a 3.5" square surface which is 47" long. The connection to the upstream and downstream vacuum system consists of a 6" adaptor plate and a spool to connect to a 4" bellows with a 4" quick disconnect at the ends of the bellows.

The vacuum liner serves as the primary absorber. It is designed to provide an impact point for the intercepted beam with low outscattering. A tapered portion is provided at the upstream end to increase the penetration of intercepted particles. This chamfer is 8.94" long with a taper of 2.56°. We expect the beam which strikes the collimator to be most intense at the downstream end of this chamfer. The wall thickness of 0.75" in the body is only 0.35" at the upstream end. Particles parallel to the collimator axis will strike the chamfer at 45 milliradian angle.

Two grooves of 0.125" width are cut in the top and bottom of the absorber block at 0.75" left and right of the centerline for mounting thermocouples. These grooves extend from the downstream end to within 19.84" of the upstream end which places them 10.9" downstream of the end of the tapered portion. For each collimator, we will instrument two channels of thermocouple readout with the other two devices available as spares.

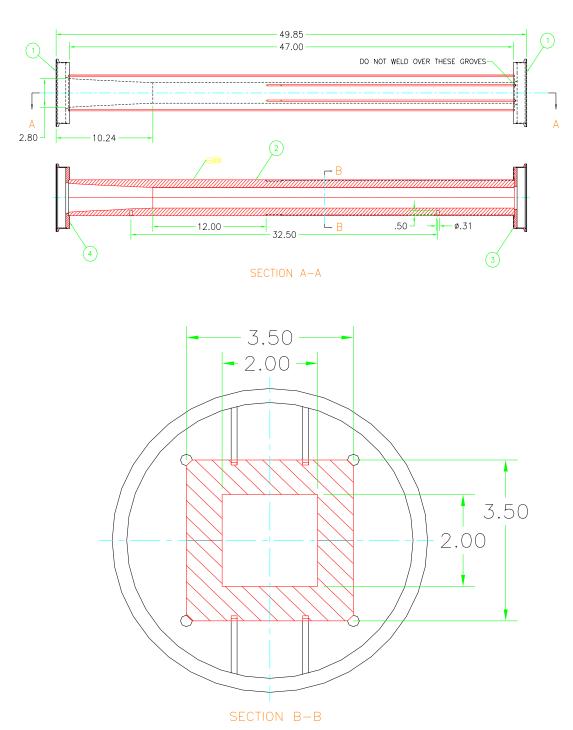


Fig.3 Stainless Steel Vacuum Liner

1- 6" Booster QD Flange; 2 – Tapered Block; 3 – End Plate DS; 4 – End Plate – US.

Vertical Motion System.

The vertical motion system is mounted on the collimator base plate.

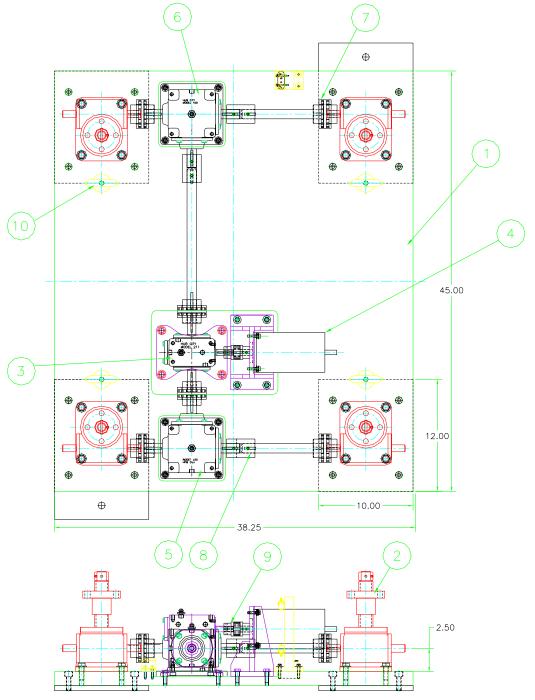


Fig. 4 Vertical Motion System.

1 – Base Plate; 2- Jack J5; 3 – Hub City 211 Gear Box, 40:1; 4 - Empire Magnetics U-42 Motor; 5 - Hub City 150A Gear Box; 6 - Hub City 150B Gear Box; 7 – Chain Coupling Assembly; 8 – Boston CR-16 Coupling; 9 – FC15 Coupling Assembly; 10 – 1.25 ton Swivel Hoist Ring.

Four J5 – five ton capacity jacks (item 2) are bolted to the base plate and connected to the drive system by couplings (items 7, 8, 9) and 1" diameter shafts. The drive system consist of Empire Magnetic U-42 step motor (item 4) and Hub City gear boxes model 211, ratio 40:1, (item3), model 150A (item 5) and model 150B (item 6) ratio 1:1. The step motor provides 71in-lb starting torque (series connection) and 48 in-lb parallel connection. Royal Purple Industrial oil SYNFILM 68 is used in all gear boxes for the lubrication



Fig. 5 Vertical Motion System, pictures.

Horizontal Motion System

The horizontal motion system is mounted on the support plate (item 1).

The support plate is bolted to the J5 vertical motion system jacks and holds a collimator absorber with vacuum liner (see fig.7). The push- pull force is provided by two ton capacity UNI-LIFT jack, J2 (item 2). The movement is plus-minus 1" from center of the beam. The torque is transferred from the motor U42 to the jack through Hub City gear box model 131, ratio 15:1.

2.7 ton capacity THK ball bearings (item 8, fig.7) are sitting on the rails (item 8, fig. 6) and are used for horizontal movement. The coefficient of friction between ball bearing block and rail is 0.05.

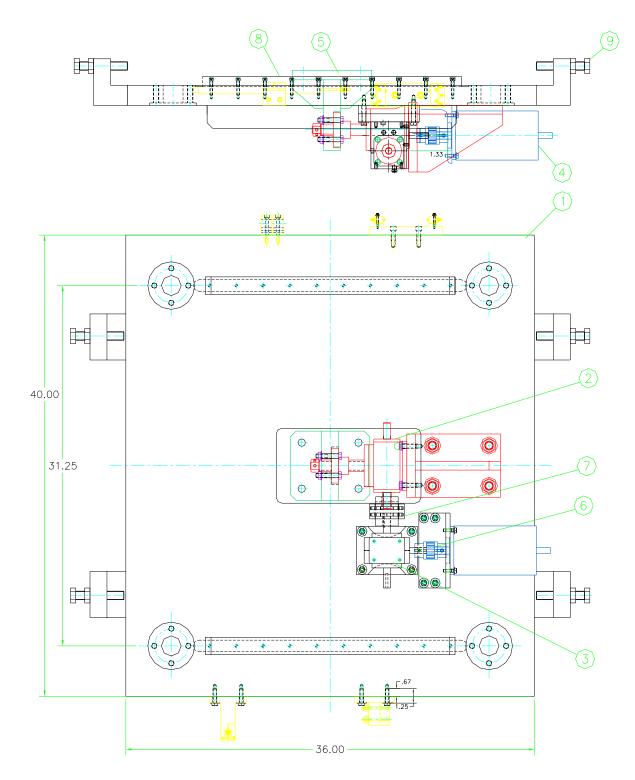


Fig. 6 Horizontal Motion System.

1 – Support Plate; 2- Jack J2; 3 – Hub City 131 Gear Box, 15:1; 4 - Empire Magnetics U-42 Motor; 6 – FC15 Coupling Assembly; 7 – Chain Coupling Assembly; 8 – THK Rail, 9 – Hard limit screw.

Steel Absorber with vacuum liner and ball bearings.

The steel absorber is assembled from steel blocks (items 2,3,4,5) that are bolted to each other and to absorber plate weldment (item1). The vacuum liner (item 6) is surrounded by steel blocks. Four thermocouples (item 7) are glued into the vacuum liner thermocouples slots (see below). Total weight steel absorber with vacuum liner is 5750 lb.

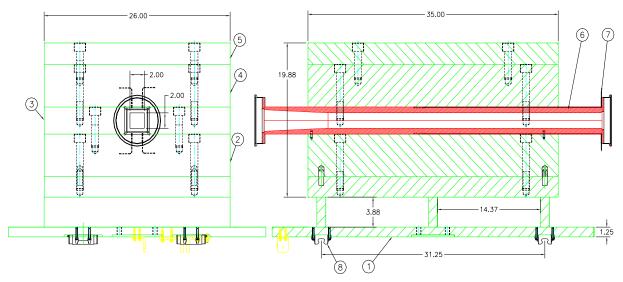


Fig. 7 Steel Absorber with THK ball bearing blocks.

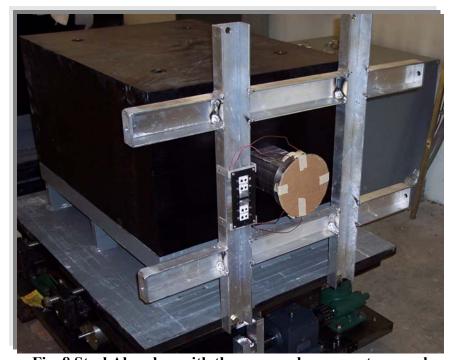


Fig. 8 Steel Absorber with thermocouples connector panel.

Marble absorber

Four layers of the marble plates 30mm (1.18") thick are placed on the absorber plate weldment and on the top of the steel absorber. Three layers of marble are inserted into the absorber plate weldment. The successful bidder provided marble from Carrara, Italy. An aluminum frame holds the marble in a place around the steel absorber. Total marble weight is 2802 lb.

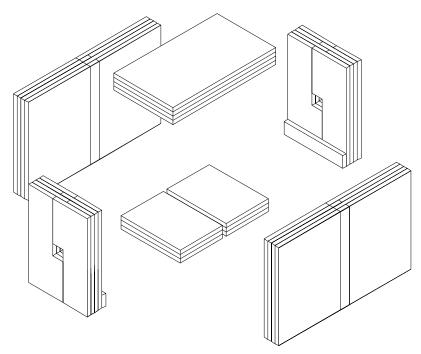


Fig. 9 Marble plates.



Fig. 10 Marble plates are inserted into absorber weldment.



Fig.11 In order to hold marble, stainless steel flat springs are installed between marble and frame.



Fig. 12 Assembled marble with aluminum frame.

Collimators location

Collimators are installed into 8-Gev line in pairs. The first pair of collimators (C1 and C2) is installed in an area between 836-837 magnets. The second pair (C3 and C4) is installed between 838-839 magnets.



Fig.13. First pair of collimators location.



Fig.14. Second pair of collimators location.

Collimators installation

175 inches of vacuum pipe is cut to prepare a space for collimators.



Fig.15 Pair of collimators is installed into beam pipe cut out.



Fig. 16 Four inch diameter STANDARD welded bellows, 10.25" long joints both collimators in pair with BOOSTER 6" diameter quick release clamps.





Fig. 17 Vacuum line in the upstream end of collimators.

The vertical BPM is welded into the vacuum pipe in the upstream end of the collimation system. STANDARD 4" welded bellows 7.5" long is connected to the BPM and collimator with BOOSTER quick release clamps (see Fig.17)





Fig. 18 Vacuum line in the down stream end of collimators

The marble mask is installed in the down stream end of the collimation system. The horizontal BPM is welded into the beam line downstream of the marble mask. STANDARD 4" welded bellows, 7.5" long is connected to the vacuum pipe and collimator with BOSTER quick release clamps. A beam loss monitor is clamped to the aisle side of the marble mask (see Fig. 18) and another is on the wall nearby. Final BLM placement will be established operationally.

Marble mask

The marble mask is assembled from six marble plates 9"x 12" x 1.25" (item2) and four bars 2" x 12" x 1.25" (item 3). Marble plates surround the Recycler-style elliptical beam pipe (item 6) and clamp to the stand (item 1) with the top plate (item 4) and threaded rods (item 5), see Fig.19.

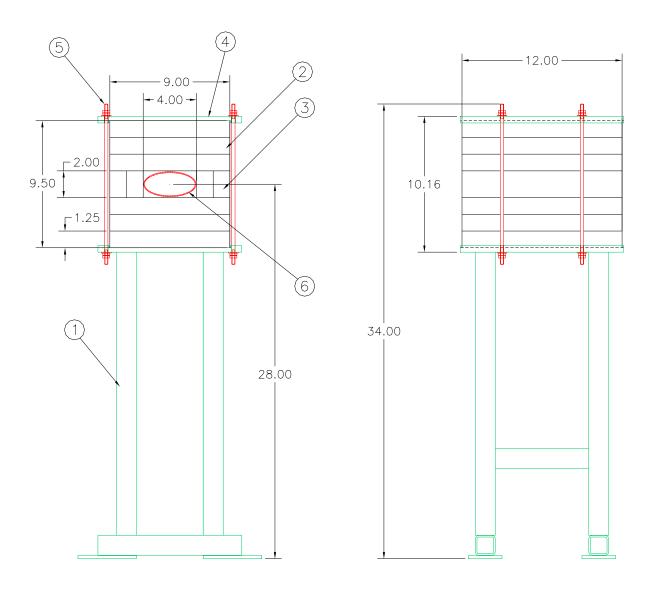


Fig.19 Marble mask assembly

Thermocouple Monitoring System

Four thermocouples (item 7 - OMEGA part #: XCIB- J -4 -3 -10) are glued into the vacuum liner thermocouple slots (see Fig.7). Upstream ends of thermocouples are located ~12" down stream from a collision point. Down stream ends of thermocouples are connected to ceramic OMEGA connectors that mounted into the panel in the down stream end of the collimator. An additional thermocouple (OMEGA part #: 5TC-GG-J -24-36) is installed for each collimator. It is initially mounted on the wall side of the vacuum liner upstream of the marble. Following thermal studies, one or more of these thermocouples may be mounted on an upstream magnet to monitor tunnel temperature. From the OMEGA connector, thermocouple wire is installed to the rack in the MI8 service building. Assignment of the OMEGA connectors is uniform for the four collimators.

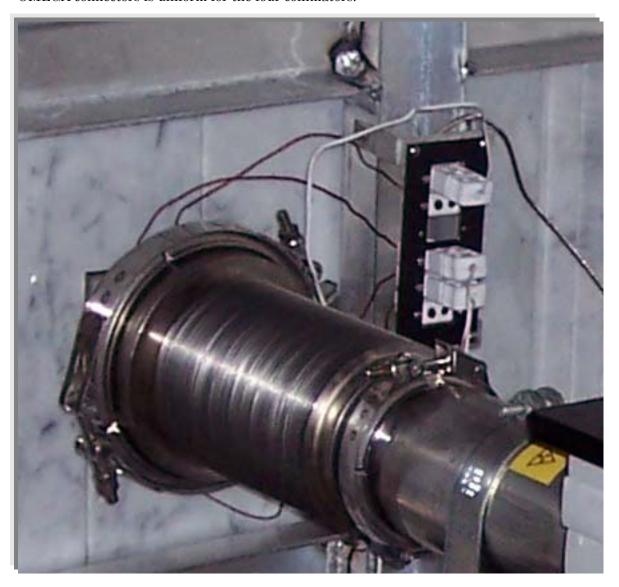


Fig.20 Thermocouple connectors panel.

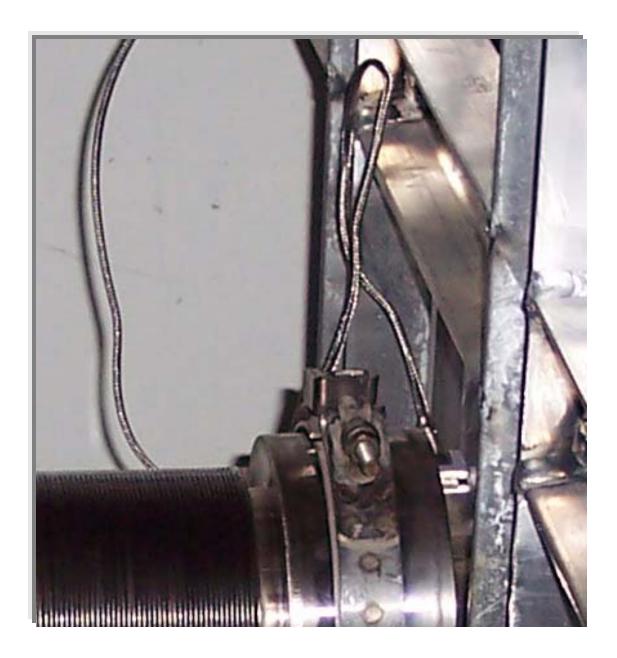


Fig.21 Front vacuum liner thermocouple.

Temperature read back

Type J thermocouples are being read by using a INOR brand # APAQ-LC Thermocouple Signal conditioner DIN rail type modules (See FIG.22) using the 10 mV input for Type J. This means the output will go to 200 Deg C. Maximum. This is the finest resolution this device offers. If studies require measurement of higher temperature, we can select a less sensitive range. The signal conditioners are then wired into the controls system CAMAC MADC system using Channels #48-59.



FIG.22 – 12 Channels of Thermocouple Couple Signal Conditioner. 3 Channels for each Collimator.

Thermocouple Placement and Assigned Channels

OMEGA	Thermo-	Collimator	Collimator	Collimator	Collimator	
Connector	couple	1	2	3	4	
	_	(836US)	(836DS)	(838US)	(838DS)	
1	Upstream	C1TC03	C2TC03	C3TC03	C4TC03	
2	Top/Wall	C1TC01	C2TC01	C3TC01		
3	Top/Aisle				C4TC01	
4	Bottom/Aisle	C1TC02	C2TC02	C3TC02		
5	Bottom/Wall				C4TC02	

On a console parameter page, these devices appear as follows:

I:TC36AT	Thermocouple 36A Top
I:TC36AB	Thermocouple 36A Bottom
I:TC36AU	Thermocouple 36A Upstrm
I:TC36BT	Thermocouple 36B Top
I:TC36BB	Thermocouple 36B Bottom
I:TC36BU	Thermocouple 36B Upstrm
I:TC38AT	Thermocouple 38A Top
I:TC38AB	Thermocouple 38A Bottom
I:TC38AU	Thermocouple 38A Upstrm
I:TC38BT	Thermocouple 38B Top
I:TC38BB	Thermocouple 38B Bottom
I:TC38BU	Thermocouple 38B Upstrm

They are currently displayed on parameter page I59 <22>.

Collimator Motion Control Hardware

The following Hardware description is associated with the 4 MI-8 Collimator motion control and position readback. The motion controls as well as the position read backs are VME based using a Motorola Power PC and various Industry Pack (IP) modules for all controls and position monitoring there is also one interface chassis and 1 interface card. The electronics is installed in rack MI08103.

The complete motion system consists of the following hardware:

- 1 VME based Motorola Power PC module MVME2430. (Front-End)
 Connected to Accelerator Controls Network (Acnet). Ethernet Node name is 'MI8CL1' (Fig. 25)
- 1 IP 16ADC 16 Channel 16 bit A/D Module from SBS Technologies
- 4 IP-STEPPER Dual Channel Stepper Module from SBS Technologies
- 1 IP-UCD Fermi Universal T-Clock Decoder. (FermiLab built)
- 2 VME based IP carrier board, the first carrier board holds 1 'IP-UCD' and 1 16 Channel A/D 'IP-16ADC', the second board holds 4 IP-STEPPER modules. (Fig. 25)
- 1 16 Ch. Motion Controls interface Chassis. (FermiLab built) (Fig. 28)
- 1 VME interface PC board that will allow analog inputs into the IP 16ADC module. (Fig. 31)
- 8 LVDT from Macro sensors 'HAS 750-1000'
- 8 LVDT Din Rail Mounted Signal Conditioners from Schaevitz. 'LDM-1000' (Fig. 29)
- 1 8 channel ACS (Advanced Control Systems) Step/Pak type chassis with 8
 SPD6B Bipolar DC Stepper motor Controller modules 6 Amps @ 48 Volt. (Horizontal and Vertical motion) (Fig. 26)
- 1 ACS SPT-8R Motor Power Transformer 48 VAC nominal (Fig. 27)

Motors Types and Specifications

- Empire Magnetics Model #RH-U42 (radiation hardened). These motors have been tested and proven to withstand >109 RADS gamma radiation for prolonged periods. (See Web Article) http://www.empiremagnetics.com/articles/rad_intensive.htm
- Motors are controlled using bipolar type drive units.
- Motors are configured with 8 wires (4 windings). Vertical motors are wired in a Series configuration to get the maximum torque output. Horizontal motors are wired in a Parallel configuration.
- The vertical motors run at a speed of 2 Revolutions per Second (RPS) which will obtain ~1300 Oz. In. of torque @ 48 Volts.
- The horizontal motors will run at a speed of 4 RPS which will obtain ~700 Oz. In. of Torque @ 48 Volts.

- Motor resolution is based on the gear reductions of the Jack Screws and other associated gear boxes. All of the motors run in half step mode / 400 Steps per Revolution.
- Each collimators vertical resolution: .001" = 576 motor steps
- Each collimators horizontal resolution: .001" = 192 motor steps.

Limit Switches

- Honeywell 2HT1 High temperature Limit Switches.
- Limit switches are wired using the normally closed contacts.
- Switches are wired through the Fermi 16 Ch. Motion Control Chassis and into the IP-Stepper modules. The Switches prevent the motors from moving, when the limit switch is opened, unplugged, or have broken wires.
- Switches are made of Aluminum and ceramic. All materials inside and outside of these switches are radiation resistant materials. (see Fig.23)



FIG.23

A hard limit on the vertical motion is provided by the nuts at the top and bottom of the jack screws. Bolts to limit the horizontal motion can be inserted in available threads on the support plate.

Position read back

- 8 LVDT's are used for position read backs. They have a maximum stroke of 2.00" (See Fig.24).
- LVDT's are read back using a Schaevitz LDM-1000 LVDT signal conditioner. The Signal conditioners produce a 0-10 VDC output signal linear to the position of the transformers core. Each signal conditioner is calibrated then connected into an analog channel in the 'MI8CL1' Front-end using one of its available 16 A/D channels. (See Fig.29)



Fig.24 - LVDT

Motion Control Relay Rack Front View.



Fig.25 - VME Crate with all Support Cards



Fig.26 – ACS Stepper Motor Controller Chassis – 8 Channels

Front View of Relay Rack



Fig.27 – 48 Volt Motor Power Supply



Fig.28 – Motor Controller Interface

Motion Control Relay Rack Back View.



Fig.29 – LVDT Signal Conditioners



Fig.30 – 16Channel Interface Chassis.



 $Fig. 31-A/D\ input\ Interface\ Board.$



Fig.32 Vertical and horizontal motion systems motors.

			MI-8 Collimator Motion Data					
ACNET Name	Motor #	Direction	Steps Per Mil	Total Pulses / 2"	Total Mils LS to LS	Backlash in Steps	Backlash in Mils	Pulses to Center
I:C836A H	0	Horizontal	192	374,840	1,952	384	2	187,804
I:C836AV I:C836BH	1 2	Vertical Horizontal	576 192	1,137,746 376,219	1,975 1,959	1,900 384	3.3	570,773 188,493
1:C836BV	3	Vertical	576	1,137,708	1,939	2,468	4.2	571,322
I:C838A H	4	Horizontal	192	379,724	1,977	1,456	7.5	191,318
I:C838AV	5	Vertical	576	1,136,854	1,973	2,080	3.6	570,507
I:C838BH	6	Horizontal	192	374,835	1,952	494	2.5	187,911
I:C838BV	7	Vertical	576	1,146,373	1,990	2,877	5	576,063

BPM system

The MI8 line BPM system includes a position monitor at each half cell. Horizontal detectors are installed at the 836 and 838 cell boundaries and vertical detectors at the 837 and 839 locations. These are of the design known as 8GeV-Line BPM (Drawing 9502.000-MB-337360-A) (A description and some measurement data for NuMI are available in Beams-doc-1412 [6]). The mechanical design employs a tube with a diagonal cut to provide sensitivity in one plane. The installation orientation determines the plane of sensitivity. The inside diameter of these BPM's is 3.870". To assure our knowledge of the beam position through the collimators, we include a BPM to measure the vertical beam position at the upstream end of the collimation space and one at the downstream end to measure the horizontal position. The complement of beam position measurements now consists of HP836, VP836(new), HP837(new), VP837, HP838, VP838(new), HP839(new), VP839. The electronics for the MI8 Line beam position is being replaced following the Spring 2006 shutdown and these new devices are temporarily being read by a test crate of the new electronics. When the electronics upgrade is complete, the full complement of position information will be available for use in an auto-tune program to limit position drift. In a separate upgrade of the MI8 Line during this shutdown, new "Texas" multiwire beam profile monitors were installed. The MI836 multiwire is now of this new type.

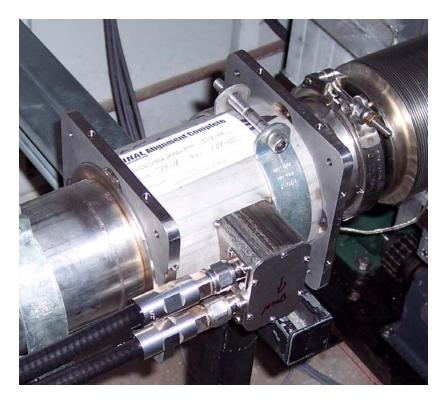


Fig.33 BPM in the vertical position, upstream end.



Fig.34 BPM in the horizontal position, down stream end.

<u>Alignment</u>

Precision knowledge of the collimator location is provided by referencing the top and side surfaces of the vacuum liner. Using this reference, the collimators were aligned to the MI8 design centerline. Since those surfaces will be difficult to access do to interference from the aluminum frame which holds the marble, alignment reference plates were installed on the aluminum frame. Four are attached the collimator top and four on the aisle side (see photo in Figure 17). These plates will be available for future precision alignment. For quick confirmation of the alignment, measurements between fixed and movable portions of the collimator system were made using rulers and stick micrometers (vertical) or electronic calipers (horizontal).

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